

thyssenkrupp Materials (UK) Ltd

Stainless Steel 1.4845

Material Data Sheet

This data sheet applies for hot and cold rolled sheet, strip and bars, semi-finished products, rods and sections as well as for seamless and welded steel tubes for mechanical and general engineering purposes.

Application

For construction parts which should be resistant to scaling up to about 1050°C and extensively inured to the effect of sulfurous gases, especially above 900°C, is very low.

Chemical Composition (heat analysis in %)

Product Form	С	Si	Mn	Р	S	Cr	Ni	N
C, H, P, L	≤ 0.10	≤ 1.50	≤ 2.00	≤ 0.045	≤ 0.015	24.00 - 26.00	19.00 - 22.00	≤ 0.11
T _{w/s*}	≤ 0.15	≤ 0.75	≤ 2.00	≤ 0.45	≤ 0.030	24.00 - 26.00	19.00 - 22.00	-

C = cold-rolled strip H = hot-rolled strip P = hot rolled sheet L= semi-finished products, bars and sections T_w = welded tubes T_s = seamless tubes * according to DIN EN 1026-2;2005-02 / DIN EN 10297-2;2007-06

Mechanical Properties (at room temperature in annealed condition)

Product Form	Thickness a or diameter d mm	HB max. ^{1) 2) 3)}	Proof Strength ³⁾		Tensile Strength	Elongation min. in %		
			R _{p0.2} N/mm²	R _{p1.0} N/mm²	R ^m N/mm ²	Long Products 3)	Flat Products	
							0.5 ≤ a/d < 3	3 ≤ a/d
C, H, P	a ≤ 12	192	210	250	500-700	35 ¹⁾	33 ⁴⁾⁵⁾	35 ⁴⁾⁵⁾
L	d ≤ 25	192	210	250	300-700	357	33 %	35 %
T _{W/S*}	-	-	230	270	min. 500	33 ^{4)/} 35 ⁵⁾	354)5)6)	354)5)6)

¹⁾ The maximum HB values may be raised by 100 units or the maximum tensile strength value may be raised by 200 N/mm² and the minimum elongation value be lowered to 20% for cold worked sections and bars of ≤ 35mm thickness.

Creep Properties (estimated average values about the long-term behaviour at elevated temperature*)

	1% Elong	ation¹) for	Rupture ²⁾ for			
Temperature °C	1,000 h N/mm²	10,000 h N/mm²	1,000 h N/mm²	10,00 h N/mm²	100,000 h N/mm²	
600	100	90	170	130	80	
700	45	30	80	40	18	
800	18	10	35	18	7	
900	10	4	15	8.5	3	

¹⁾ Stress related to the output cross section, which leads after 1,000 or 10,000 h to a permanent elongation of 1%.

²⁾ For quidance only.

³⁾ For rod, only the tensile values apply.

⁴⁾ Longitudinal test piece.

⁵⁾ Transverse test piece

⁶⁾ After cold forming the elongation for wall thicknesses ≤ 35mm amounts to minimum 20%.

²⁾ Stress related to the output cross section, which leads after 1,000 or 10,000 or 100,000 h to breakage.

^{*} For guidance only



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Reference data on some physical properties

Density at 20°C	Thermal Condu	ctivity W/m K at	Specific Thermal	Electrical Resistivity at 20°C Ω mm²/m	
kg/dm³	20°C	500°C	Capacity at 20°C J/kg K		
7.9	15	19	500	0.85	

Coefficient of linear thermal expansion 10 ⁻⁶ K ⁻¹ between 20°C and						
200°C	400°C	600°C	800°C	1000°C		
15.5	17.0	17.5	18.5	19.0		

Guidelines on the temperature for hot forming and heat treatment

Hot Fo	orming	Heat Treatment ¹⁾ +A (annealed), Microstructure				
Temperature °C	Type of Cooling	Temperature °C	Type of Cooling	Microstructure		
1150 - 800	Air	1050 - 1150 ²⁾	Air, Water³)	Austenite		

¹⁾ Heat treatment is not necessary in any case, since the material is exposed to high temperatures during application.

Processing / Welding

Standard welding processes for this steel grade are:

- TIG-Welding
- MAG-Welding Solid Wire
- Arc Welding (E)
- Laser Bean Welding

Process	Filler Metal				
Flocess	Similar D	Higher Alloyed C, CM			
TIG Thermanit C Si / 1.4842 + Thermanit CR		-			
MAG Solid Wire	Thermanit C Si / 1.4842 + thermanit CR	-			
Arc Welding (E)	Thermanit C / 1.4842 + Thermanit CR	-			
Laser Beam Welding	See Page 3	-			

Preheating is not necessary for this steel. Interpass temperature should not exceed 150°C. Heat treatment after welding is normally not usual. Austenitic steels have only 30% of the thermal conductivity of non-alloyed steels. Their fusion point is lower than that of non-alloyed steels, therefore austentic steels have to be welded with lower heat input than non-alloyed steels.

To avoid overheating or burn-through of thinner sheets, higher welding speed has to be applied. Copper back-up plates for faster heat rejection are functional, whereas, to avoid cracks in the solder metal, it is not allowed to surface-fuse the copper back-up plate.

This steel has an extensively higher coefficient of thermal expansion as non-alloyed steels. In connection with a worse thermal conductivity, a greater distortion has to be expected.

When welding 1.4845 all procedures, which work against this distortion (e.g. back-step sequence welding, welding alternately on opposite sides with double-V butt weld, assignment of two welders when the components are accordingly large) have to be respected notably. For product thicknesses over 12mm the double-V butt weld has to be preferred instead of a single-V butt weld. The included angle should be 60° - 70°, when using MIG-welding about 50° is enough. An accumulation of weld seams should be avoided.

Tack welds have to be affixed with relatively shorter distances from each other (significantly shorter than those of non-alloyed steels), in order to

²⁾ If heat treatment is carried out in a continuous furnace, the upper part of the range specified is usually preferred or even exceeded.

³⁾ Cooling has to be effected fast enough.



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prevent strong deformation, shrinking or flaking tack welds. The tacks should be subsequently grinded or at least be free from crater cracks. 1.4845 in connection with austenitic weld metal and too high heat input the addiction to heat cracks exists. The addiction to heat cracks can be confined, if the weld metal features a lower content of ferrite (delta ferrite). Contents of ferrite up to 10% have a favourable effect and do not affect the corrosion resistance generally. The thinnest layer possible has to be welded (stringer bead technique) because a higher cooling speed decreases the addiction to hot cracks.

A preferably fast cooling has to be aspired whole welding as well, to avoid the vulnerability to intergranular corrosion and embrittlement. 1.4845 is very suitable for laser beam welding. With a welding groove width smaller 0.3mm respectively 0.1mm product thickness the use of filler metals is not necessary. With larger welding grooves a similar filler metal can be used. With avoiding oxidation within the seam surface during laser beam welding by applicable backhand welding, e.g. Helium as inhert gas, the welding seam is as corrosion resistant as the base metal. A hot crack hazard for the welding seam does not exist, when choosing an applicable process.

1.4845 is also suitable for laser beam fusion cutting with nitrogen or flame cutting with oxygen. The cut edges only have small heat affected zones and are generally free of micro cracks and thus are well formable. While choosing an applicable process the fusion cut edges can be converted directly. Especially, they can be welded without any further preparation.

While processing only stainless tools like steel brushes, pneumatic picks and so on are allowed, in order to not endanger the passivation. It should be neglected to mark within the welding seam zone with oleaginous bolts or temperature indicating crayons.

The high corrosion resistance of this stainless steel is based on the formation of a homogeneous, compact passive layer on the surface. Annealing colours, scales, slag residues, tramp iron, spatters and such like have to be removed, in order to not destroy the passive layer.

For cleaning the surface the processes brushing, grinding, pickling or blasting (iron-free silica sand or glass spheres) can be applied. For brushing only stainless steel brushes can be used. Pickling of the previously brushed seam area is carried out by dipping and spraying, however, often pickling pastes or solutions are used. After pickling a careful flush with water has to be done.

Remark

In quenched condition the material can be slightly magnetizable. With increasing cold forming the magnetizability increases. Heat resisting tubes are delivered regarding testing in accordance to DIN EN 10296-2 respectively DIN EN 10297-2. In Germany, SEW 470 still applies for heat resisting tubes.

Editor

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Important Note

Information given in this data sheet about the condition or usability of materials respectively products are no warranty for their properties, but act as a description.

The information, we give on for advice, comply to the experiences of the manufacturer as well as our own. We cannot give warranty for the results of processing and application of the products.